

Optimal design of 2-D and 3-D shaping for linear ITG stability*

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in collaboration with

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Overview of results

i. Design targets

- The targets provide an analytic, quantitative metric for the relation between the geometry and the ITG instability.

ii. Optimal design mechanisms

- The essential mechanisms by which the shaping controls the targets are investigated.

iii. Example calculations

- Example calculations build a framework for understanding.
- Show we can analytically predict & explain trends in the maximum linear growths rate from GENE.

Thus, a clear path to ITG optimization is shown.

A simpler approach to understanding 3-D shaping effects is needed

- **Success in neoclassical optimization has given rise to interest in turbulence optimization using shaping**
 - Linear growth rate provides a natural “cost function”
 - However, seemingly vast parameter space
 - What and how we should optimize is unclear.
- **Thus we consider a simpler problem & methodology:**
 - linear ion temperature gradient mode growth rates, electrostatic, low-beta, adiabatic electrons, no flows, $\eta_i = 10$, $L_n^{-1} = 2$, $L_T^{-1} = 20$
 - local equilibrium theory -- analytic, single surface only
 - ballooning/flux-tube, and assume Gaussian modes in analytics

Central question:

- ***How does one optimize the geometric properties of a surface along a field line for ITG modes?***

A proxy function for the growth rate is derived using analytic ITG theory

- Ballooning/flux-tube limit, fluid limit $\omega/k_{\parallel} \gg v_{th,i}$, gyrokinetics theory (Romanelli 1989) yields ODE, cubic in eigenfrequency

$$\hat{\omega}^3 \left(1 + \frac{b}{L_k^2} \hat{k}_{\perp}^2\right) \hat{\phi} - \hat{\omega}^2 \frac{\sqrt{b}}{L_n} \left(1 + 2 \frac{\rho L_n}{L_d^2} \hat{\omega}_d - W_K \frac{b}{L_k^2} \hat{k}_{\perp}^2\right) \hat{\phi} + \hat{\omega} \left(-2 W_K \frac{b}{L_d^2} \frac{\rho}{L_n} \hat{\omega}_d - \frac{1}{2} \frac{\rho^2}{L_{\parallel}^2} \hat{k}_{\parallel}^2\right) \hat{\phi} - W_K \frac{\sqrt{b}}{L_n} \frac{1}{2} \frac{\rho^2}{L_{\parallel}^2} \hat{k}_{\parallel}^2 \hat{\phi} = 0$$

Geometric coefficients

- Solve by averaging over eigenfunction,

$$\langle f \rangle = \int_{\eta_i}^{\eta_f} d\eta \hat{\phi}^* f \hat{\phi} / \int_{\eta_i}^{\eta_f} d\eta |\hat{\phi}|^2,$$

$$\hat{\omega} = - \frac{\frac{\sqrt{b}}{L_n} \left(-1 - 2 \frac{\rho L_n}{L_d^2} \langle \hat{\omega}_d \rangle + W_K \frac{b}{L_k^2} \langle \hat{k}_{\perp}^2 \rangle\right)}{2 \left(1 + \frac{b}{L_k^2} \langle \hat{k}_{\perp}^2 \rangle\right)} \pm$$

Only get $\gamma = \text{Im}(\omega) > 0$
for $\langle \omega_d \rangle < 0$

$$\frac{\sqrt{\frac{\sqrt{b}}{L_n} \left(-1 - 2 \frac{\rho L_n}{L_d^2} \langle \hat{\omega}_d \rangle + W_K \frac{b}{L_k^2} \langle \hat{k}_{\perp}^2 \rangle\right)^2 + 4 \left(1 + \frac{b}{L_k^2} \langle \hat{k}_{\perp}^2 \rangle\right) \cdot \left(2 W_K \frac{b \rho}{L_d^2 L_n} \langle \hat{\omega}_d \rangle + \frac{1}{2} \frac{\rho^2}{L_{\parallel}^2} \langle \hat{k}_{\parallel}^2 \rangle\right)}}{2 \left(1 + \frac{b}{L_k^2} \langle \hat{k}_{\perp}^2 \rangle\right)}$$

Shaping controls the proxy target via the drift and FLR coefficients

- Result indicates squared growth rate scales like $\chi_{ITG}^2 = -\frac{\langle \hat{\omega}_d \rangle}{\langle \hat{k}_\perp^2 \rangle}$.

- **Drift coefficient**

$$\hat{\omega}_d = 2L_d^2 B_0 \frac{\kappa_n - \Lambda \kappa_g}{|\nabla \psi|}$$

- Normal curvature, geodesic curvature, torsion, and local shear

$$\begin{aligned} (\hat{\mathbf{b}} \cdot \nabla) \hat{\mathbf{b}} &= \kappa_n \hat{\mathbf{n}} + \kappa_g \hat{\mathbf{b}} \times \hat{\mathbf{n}} \\ (\hat{\mathbf{b}} \cdot \nabla) \hat{\mathbf{n}} &= -\kappa_n \hat{\mathbf{b}} + \tau_n \hat{\mathbf{b}} \times \hat{\mathbf{n}} \\ (\hat{\mathbf{b}} \cdot \nabla) \hat{\mathbf{b}} \times \hat{\mathbf{n}} &= -\tau_n \hat{\mathbf{n}} - \kappa_g \hat{\mathbf{b}} \\ s &= \hat{\mathbf{b}} \times \hat{\mathbf{n}} \cdot \nabla \times (\hat{\mathbf{b}} \times \hat{\mathbf{n}}). \end{aligned}$$

- **FLR/polarization coefficient**

$$\hat{k}_\perp^2 = L_k^2 B_0^2 \frac{1 + \Lambda^2}{|\nabla \psi|^2}$$

- Parallel currents, P-S currents, local shear, and integrated local shear

$$\begin{aligned} \mu_0 \frac{\mathbf{J} \cdot \mathbf{B}}{B^2} &= \sigma + p' \lambda \\ \mathbf{B} \cdot \nabla \lambda &= 2\mu_0 \frac{|\nabla \psi|}{B} \kappa_g \\ s &= \sigma + p' \lambda - 2\tau_n = \frac{g^{\psi\psi}}{B^2} \left(\frac{\iota'}{\sqrt{g}} + \mathbf{B} \cdot \nabla D \right) \\ \Lambda &= \frac{\nabla S \cdot \nabla \psi}{B} = -\frac{g^{\psi\psi}}{B} \int_{\eta_k}^{\eta} d\eta \sqrt{g} \frac{B^2}{g^{\psi\psi}} s. \end{aligned}$$

The instability scaling suggests three distinct shaping goals

Goals for shaping

1. Shift & maximize $\langle \frac{\kappa_n}{|\nabla\psi|} \rangle > 0$
2. Shift & maximize $\langle \frac{-\Lambda\kappa_g}{|\nabla\psi|} \rangle > 0$
3. Maximize $\langle \frac{\Lambda^2}{|\nabla\psi|^2} \rangle > 0$
 - a. Minimize $|\nabla\psi|^2$

Physical meanings

Curvature drive

Geodesic curvature-torsion drive

Parallel/perpendicular coupling
Shear/FLR/polarization effects

- **Note that currents, global shear, and averaged torsion all related,**

$$\sigma = -\nu\hat{s} + 2\bar{\tau}_n \quad \hat{s} = -B_0\rho^2\iota'/\iota \quad \bar{\tau}_n = \langle B^2\tau_n/g^{\psi\psi} \rangle_{fs} / \langle B^2/g^{\psi\psi} \rangle_{fs}$$

- **Goal (2) implies rules for 2-D and 3-D (weak currents)**

$$\kappa_g \cdot \int_{\eta_k}^{\eta} d\eta (\bar{\tau}_n - \tau_n) > 0 \text{ for } \kappa_n < 0 \ \& \ \hat{s} < 0 \quad \text{2-D symmetry design rules}$$

$$\kappa_g \cdot \int_{\eta_k}^{\eta} d\eta (\tau_n) < 0 \text{ for } \kappa_n < 0 \quad \text{3-D symmetry design rules}$$

Thus, relative phases of the curvatures and torsion are crucial.

Shaping mechanisms may be broadly categorized into a few general types

- **2-D: poloidal shaping (concavity & convexity control)**

$$R = R_0 + \rho_0 \cos(\bar{\theta}) + \rho_1 \cos(M\bar{\theta}) + \dots$$

- **3-D: three more fundamental mechanisms**

- Axial translation

$$R = R_0 + \rho_0 \cos(\bar{\theta}) + \rho_1 \cos(N\bar{\zeta}) + \dots$$

- Cross sectional rotation

$$R = R_0 + \rho_0 \cos(\bar{\theta}) + \rho_1 \cos(M\bar{\theta} - N\bar{\zeta}) + \dots$$

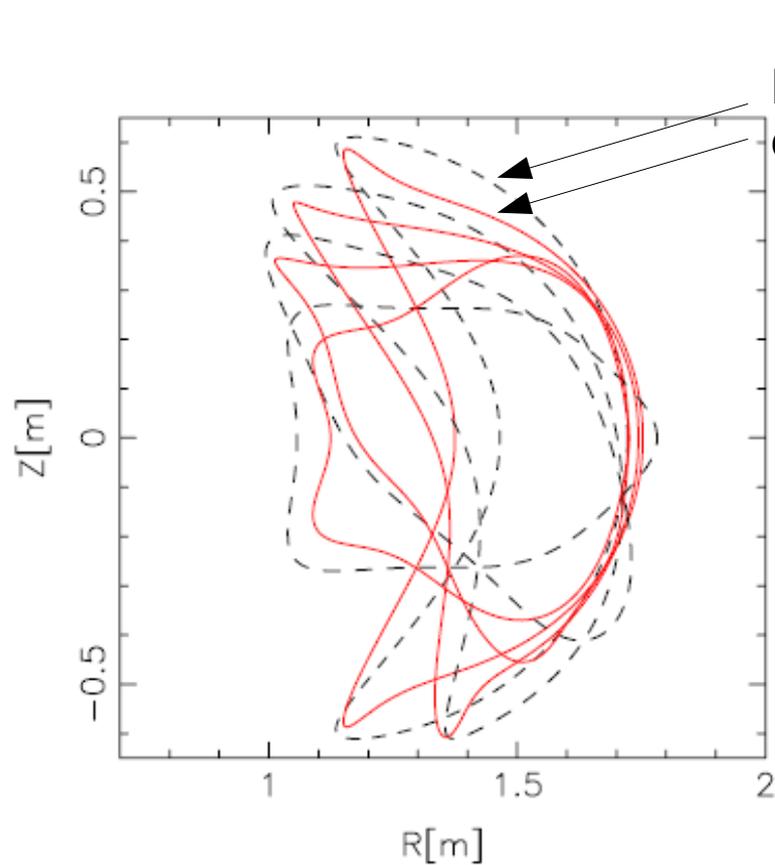
- Cross sectional deformation (e.g. w/ rotation)

$$R = R_0 + \rho_0 \cos(\bar{\theta}) + \rho_1 \rho_2 \cos(N_2\bar{\zeta}) \cos(M\bar{\theta} - N\bar{\zeta}) + \dots$$

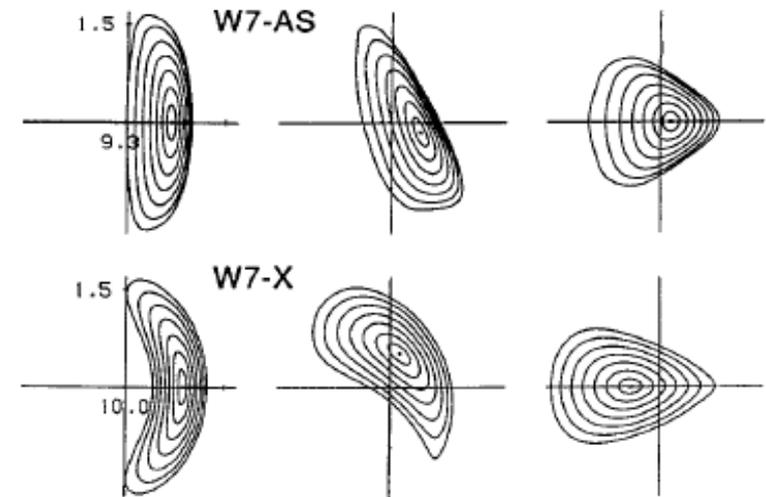
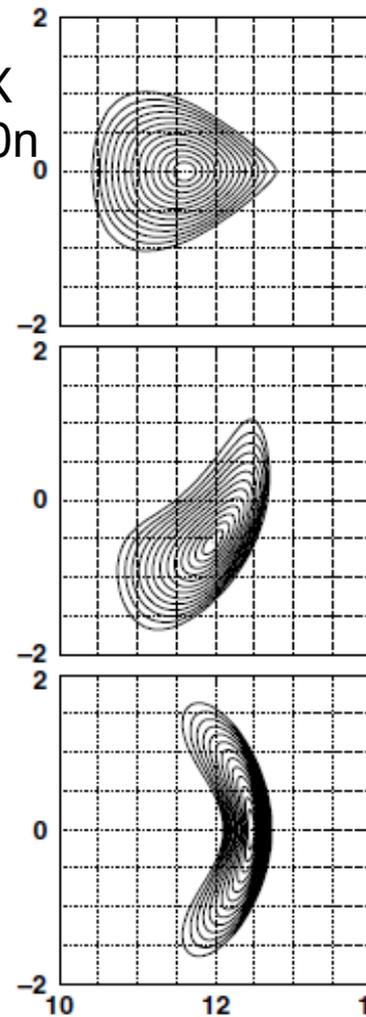
- **3-D shaping intimately tied to iota and (global) shear**

- In 2-D, constraint is broken by currents

Note optimized stellarators usually show both rotation and deformation



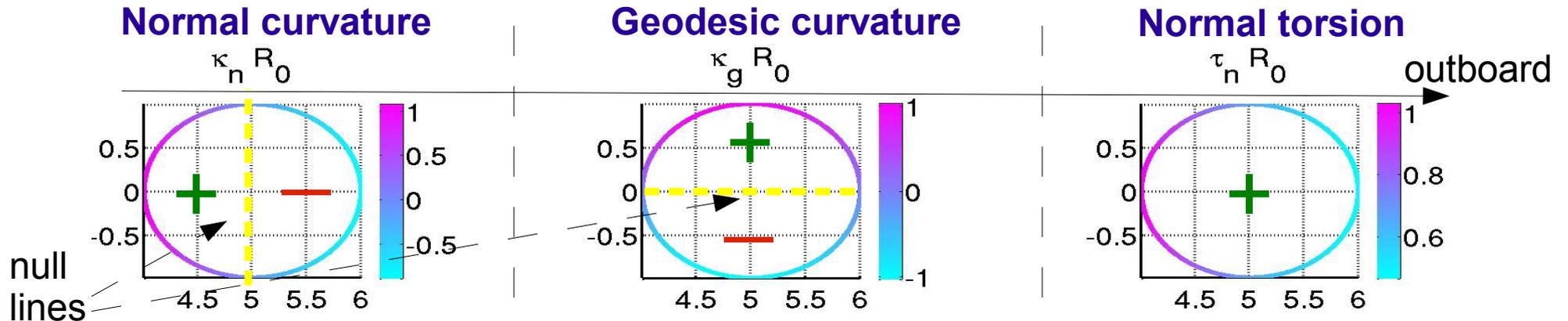
Mynick et. al., Physical Review Letters, 105 095004, 2010



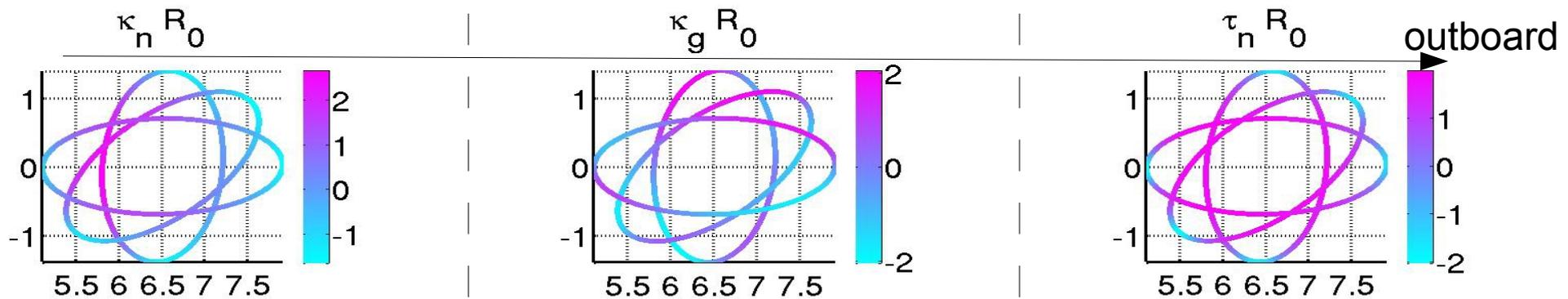
Grieger et. al., Phys. Fluids B, 4 2081, 1992

Subbotin et. al., Nuclear Fusion, 46 921, 2006

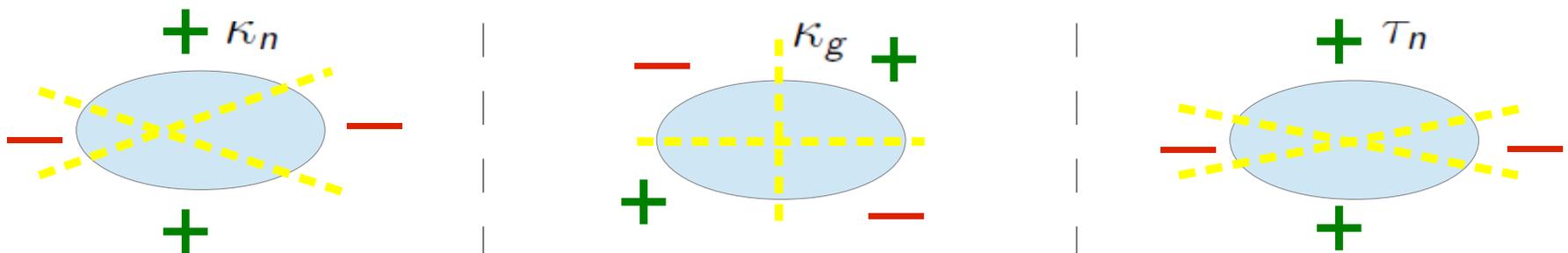
Curvature symmetries are controlled by edge positioning



In 2-D, symmetry lines are typically left/right or up/down



In 3-D, the symmetry lines follow corners/edges/cusps



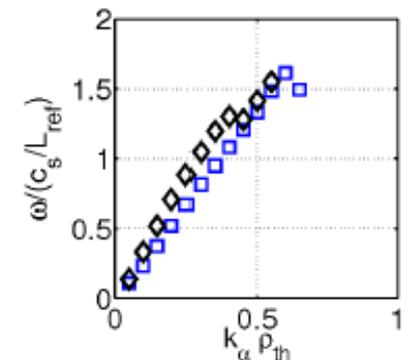
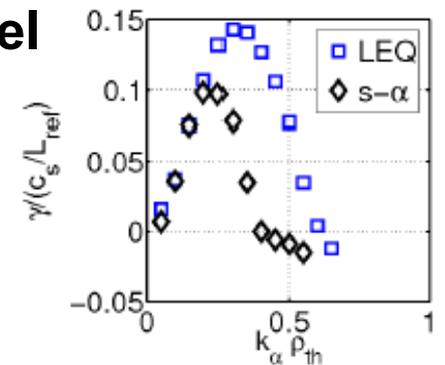
A framework for understanding is built up via selective example calculations

- Analytic proxy results compared w/ numerical gyrokinetics GENE results using same equilibrium input

- Local equilibrium method checked against s-alpha model

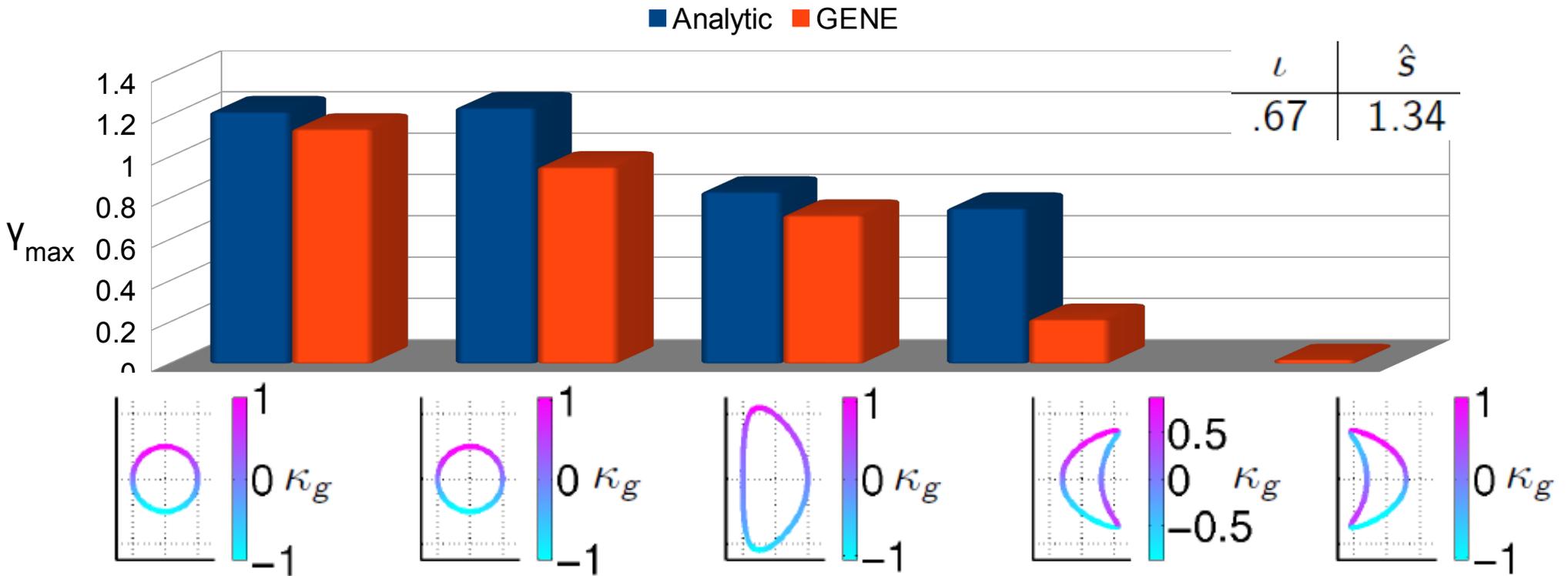
- Simplifying assumptions for the rest of results:

- high gradients, $\eta_i = 10$, $L_n^{-1} = 2$, $L_T^{-1} = 20$
- geometric angles are straight field line angles
- limitation: manual parametrization of geometries

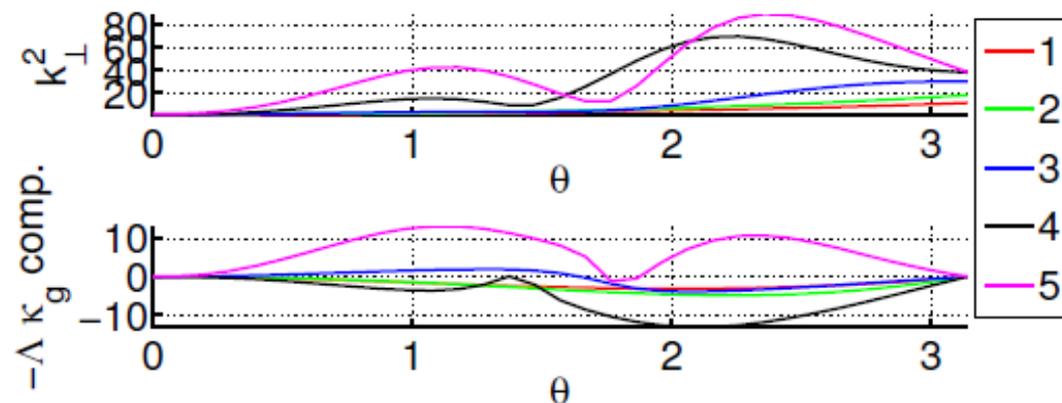


- Focus on maximum linear growth rate -- scanning over ky-rho

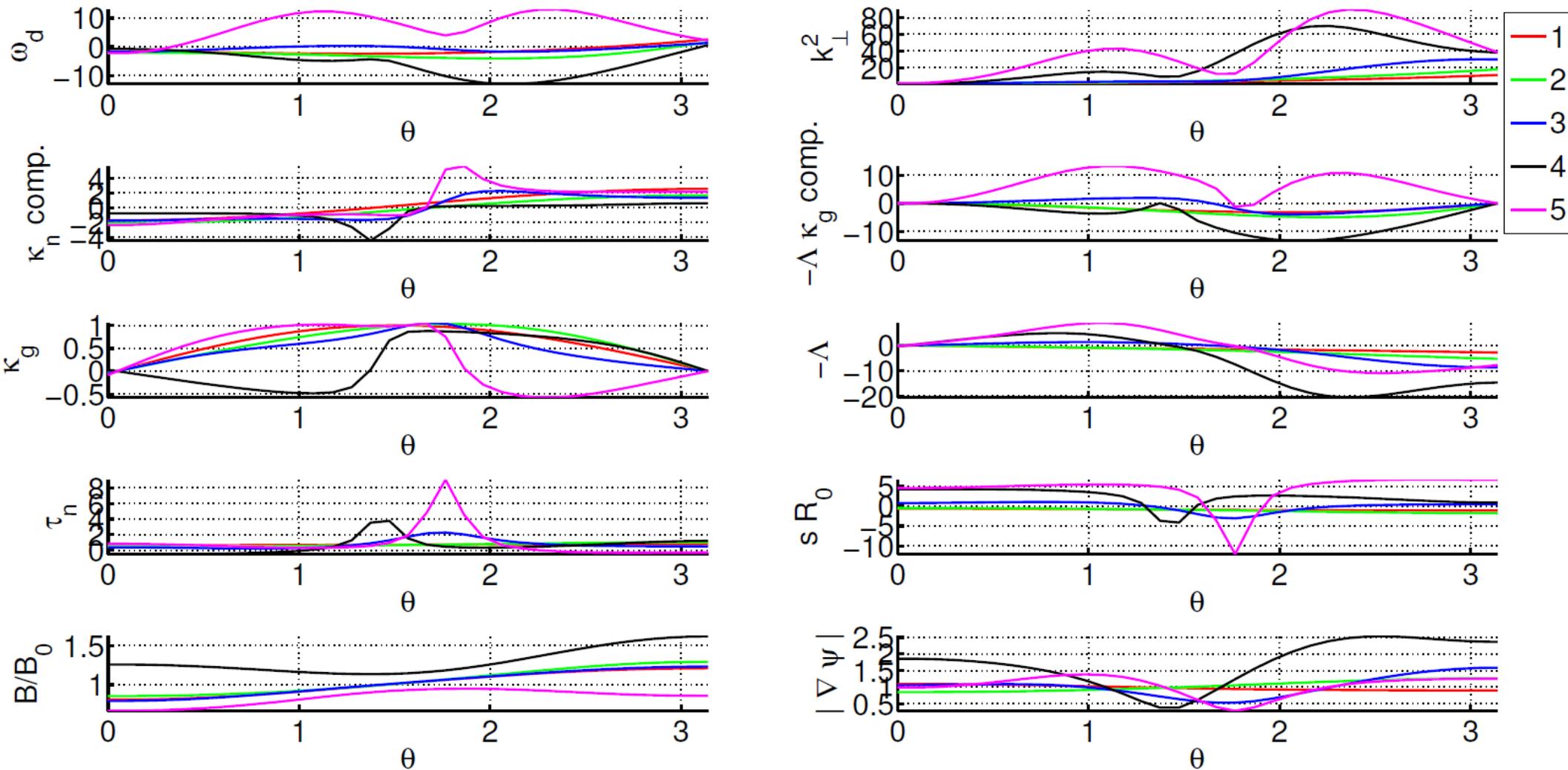
Concave inboard shaping yields both drift and FLR optimization



- More averaged torsion & currents for cases 4,5 yield larger k_{\perp}^2
- Geodesic curvature phasing is optimal for case 5 vs. case 4
- Case 4 poor agreement – kinetic effects?

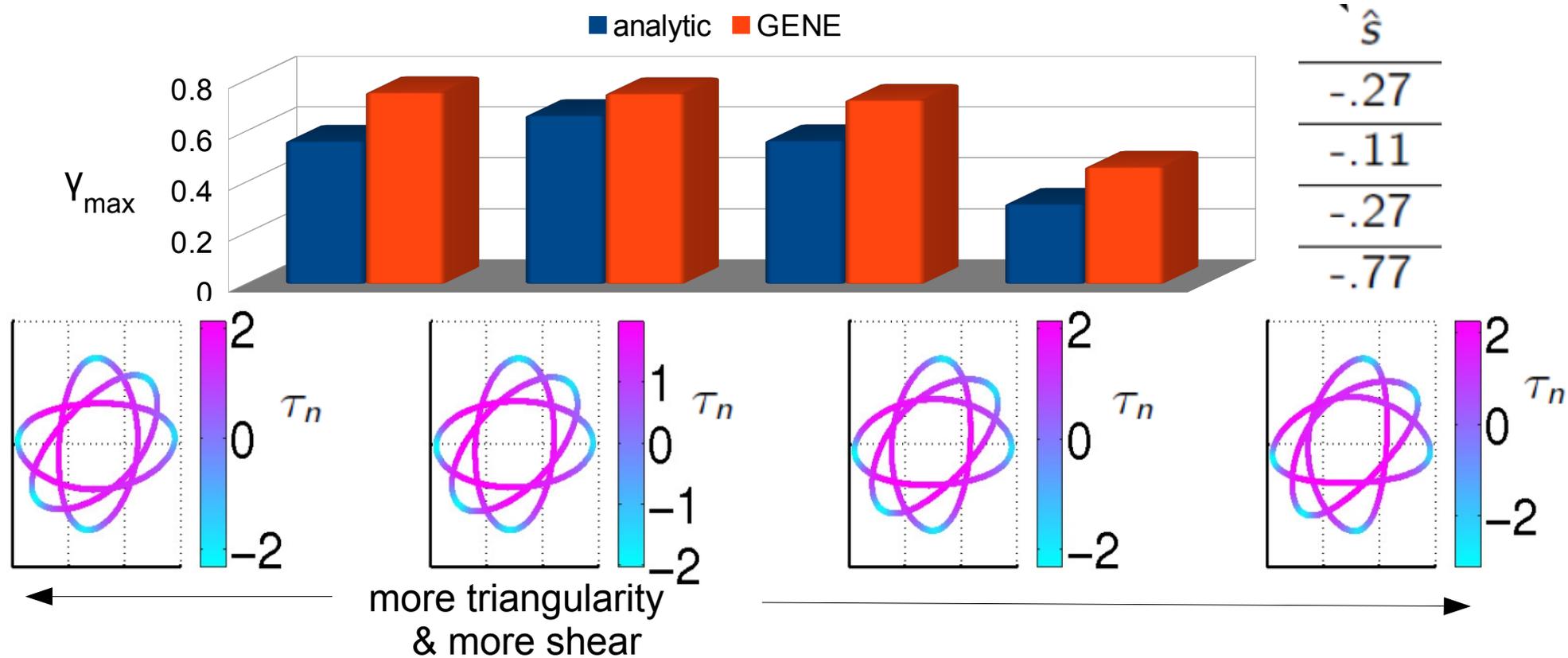


A few geometric quantities completely describe the surface



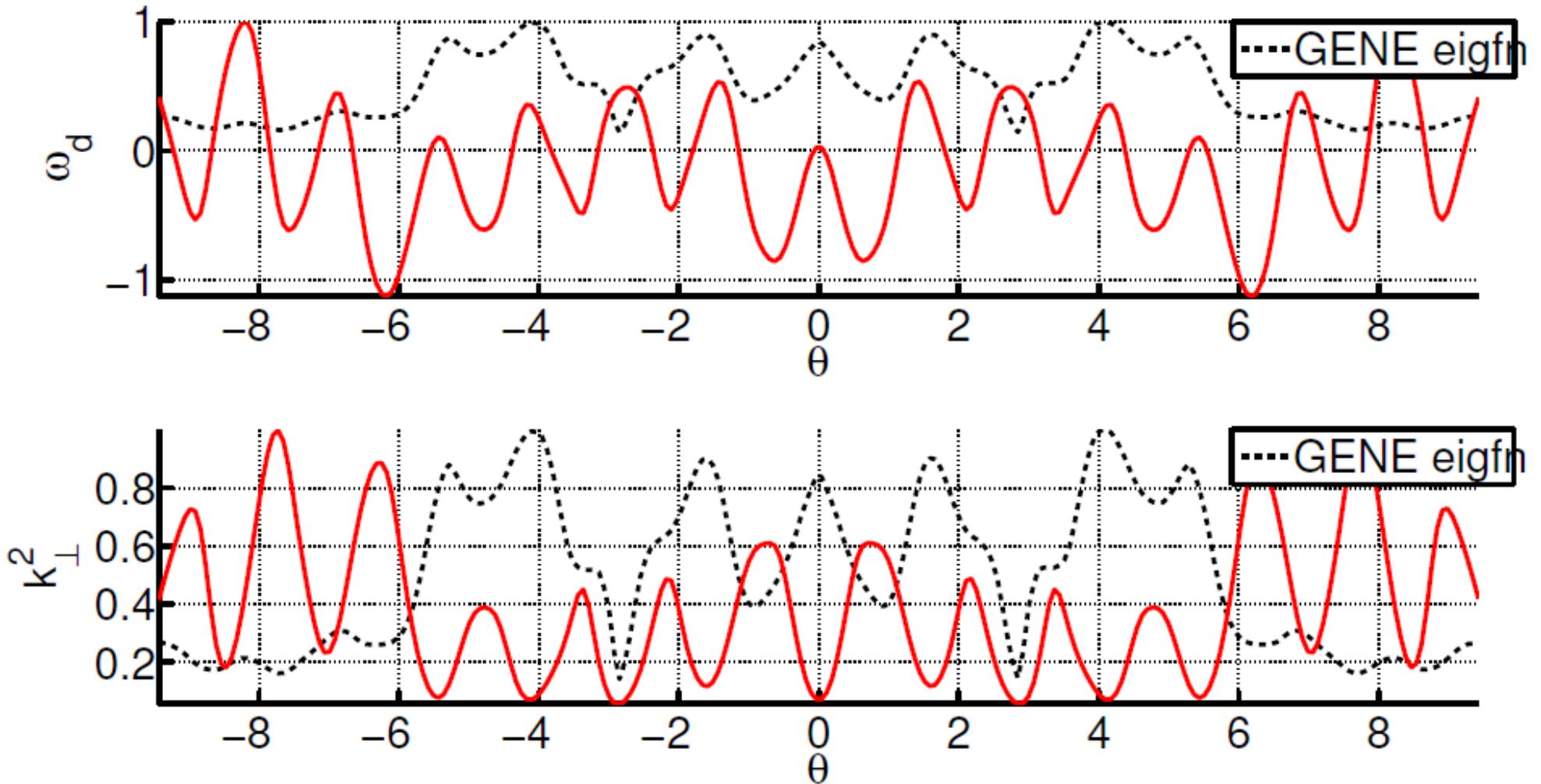
Can build intuition & completely analyze geometries with ~ 10 field line plots and handful of full surface plots.

Proxy result trends match GENE trends in stellarator geometry scans



- **GENE results from domain extending 3 poloidal circuits ($n_{\text{pol}}=3$), proxy results with Gaussian full width of 3 poloidal circuits**
- **GENE shows only ~10% difference from $n_{\text{pol}}=1$ to 3**
- **Proxy misses trend on case 2 but geometries 1, 2, 3 all very similar**

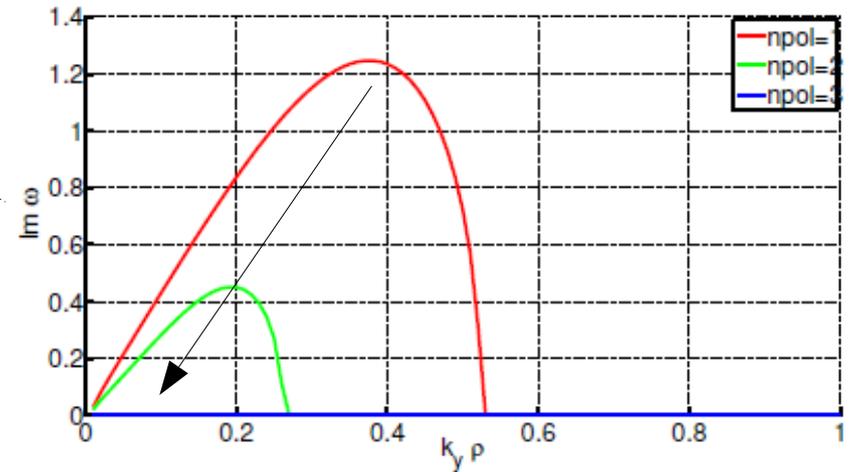
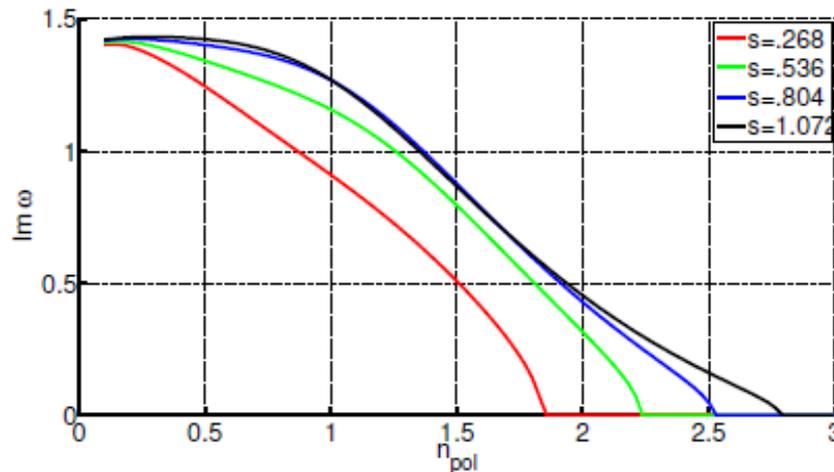
GENE eigenfunctions clearly sit in w_d wells and k_{\perp}^2 troughs



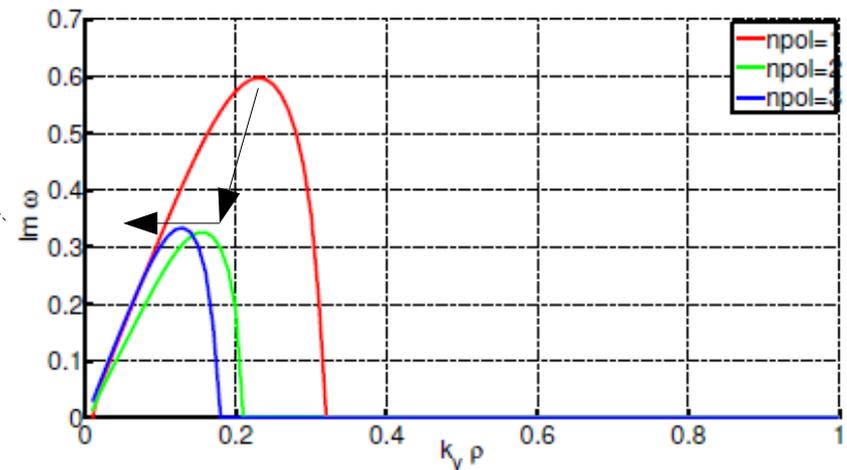
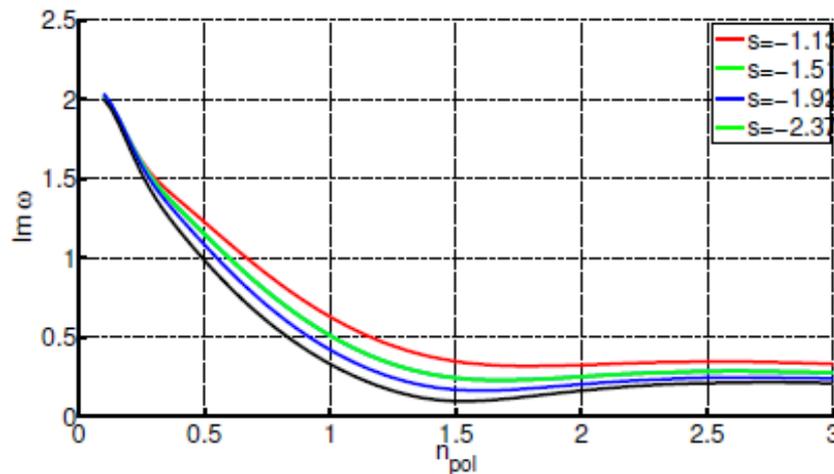
Extended GENE eigenfunction for case 2 (prev. slide), $n_{\text{pol}}=3$, against unitized values of w_d and k_{\perp}^2

The analytic proxy growth rate can be sensitive to Gaussian mode width

Shear scan, circular tokamak -- shear destabilizes due to increase in curvature drive, spectra shrink to $k_y\rho = 0$

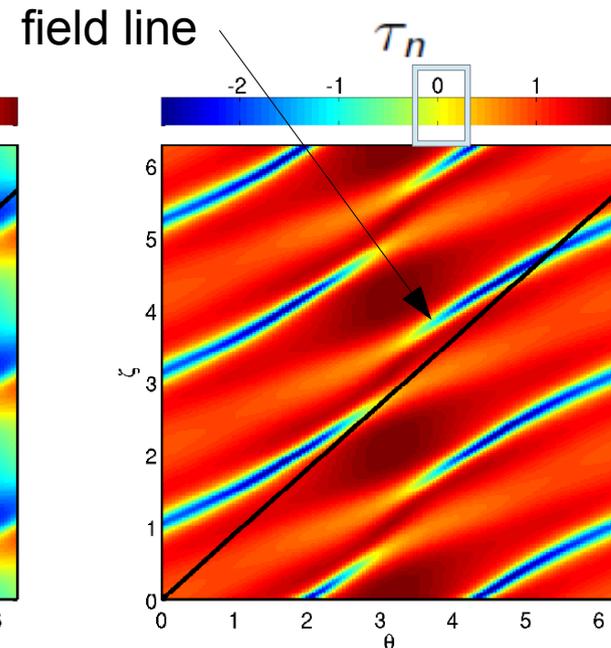
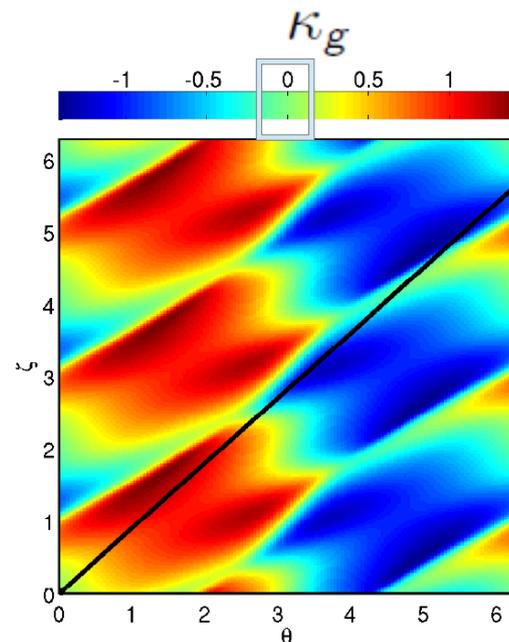
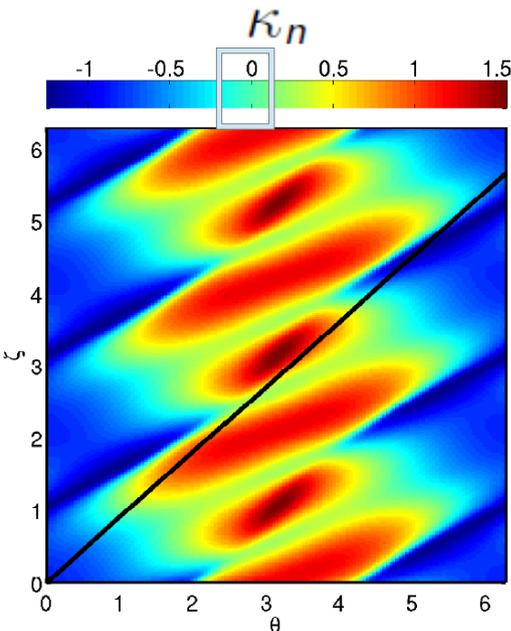
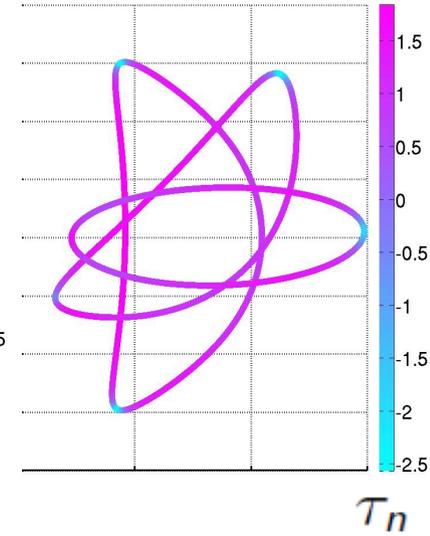
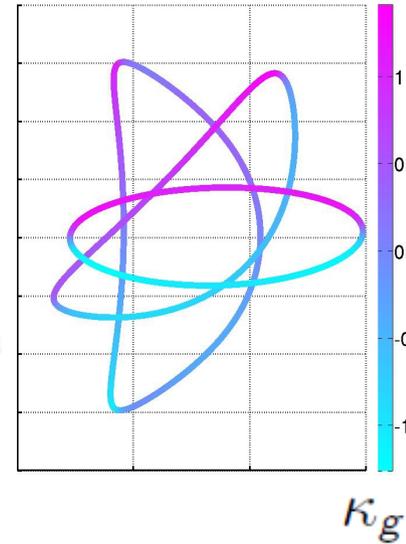
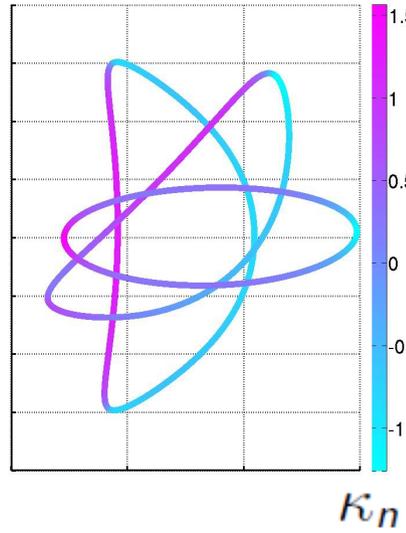
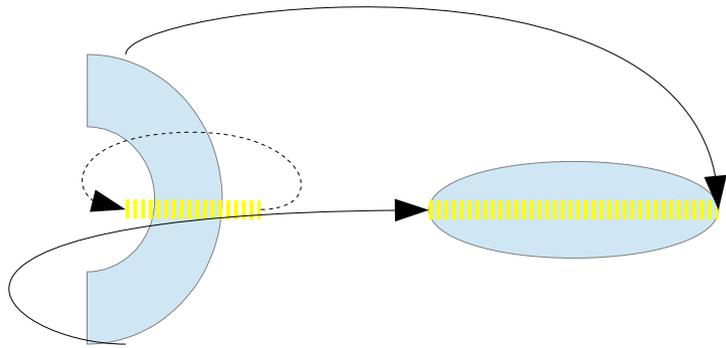


Elong. scan, N=10, m=1 stellarator -- shear stabilizes, gamma's converge due to spectral shift to smaller $k_y\rho$ & k_{perp}^2 non-monotonic



Deformation mechanism enables alteration of curvature symmetries

Deformation here causes the null lines to counter-rotate with respect to the surface



The helical curvature component is notably tuned out compared to a fixed M,N stellarator

Advanced shaping mechanisms necessitate numeric optimization

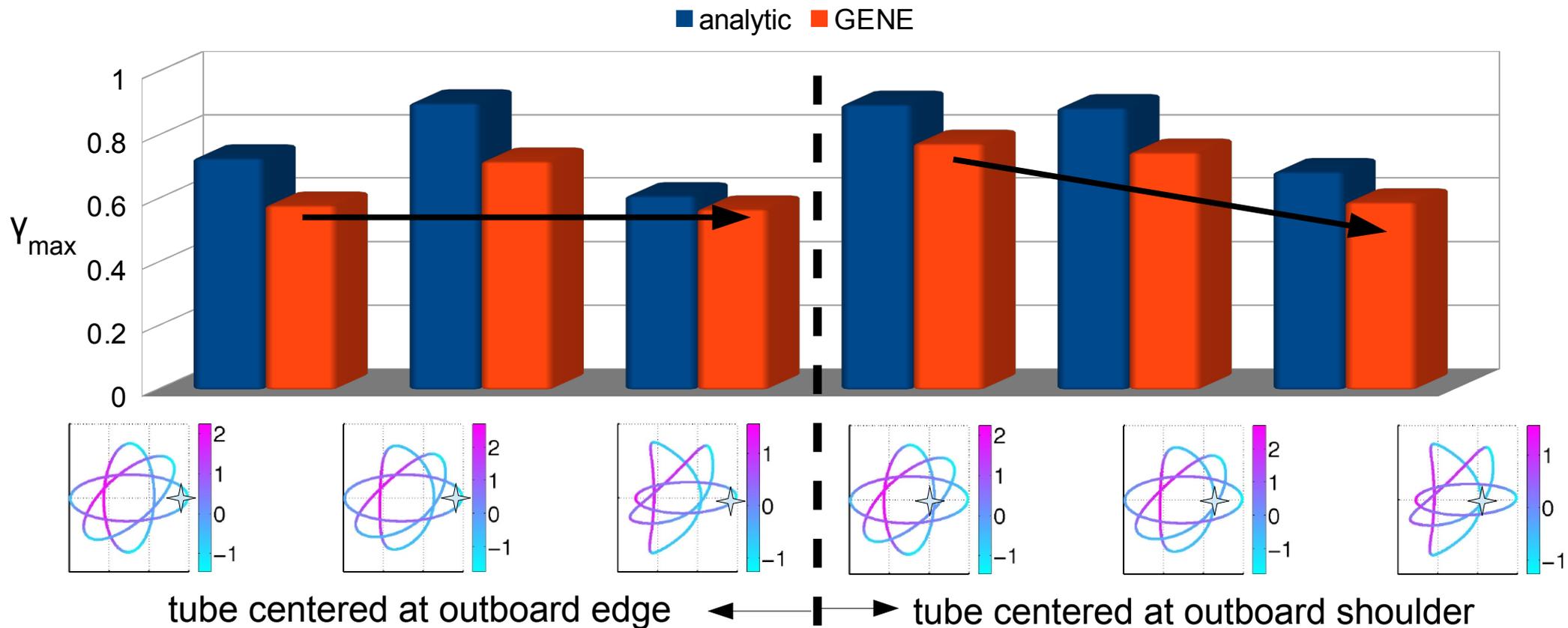
- **Local 3-D equilibrium theory developed for analytic parametrization of a single surface**
 - Good for simple shaping
 - Advanced shaping parametrizations cumbersome
- **Ex. (case from previous slide):**

$$R = R_0 + \rho_0 \cos(\theta)(1 + \rho_6 \cos(N_4\zeta)^2) + \rho_2 \cos(\theta - N\zeta) \\ + \rho_3 \cos(2\theta - N_2\zeta - \pi/2) \sin(N/2\zeta) + \rho_5 \cos(M\theta - N_3\zeta) \sin(N/2\zeta)^2 \\ + \delta \cos(N\zeta)$$

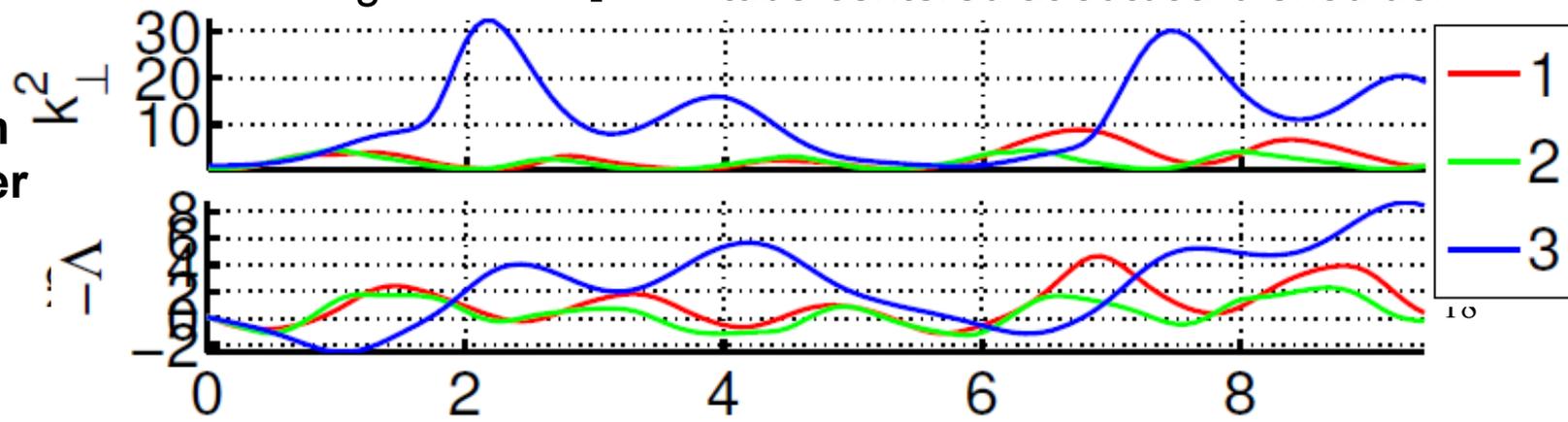
$$R_0 = 6.5, \rho_0 = 1.05, \rho_6 = -0.2, N_4 = .5N, \rho_2 = 0.4\rho_0, N = 3, \rho_3 = 0.5\rho_2, N_2 = 1.5N, \rho_5 = -0.2\rho_3, N_3 = 2N, \delta = 0.2\rho.$$

- **Harmonics:** 1 pure poloidal, deformational, rotational, and translational, and 2 simultaneous rotational + deformational

Deformation shaping improves on M=1 shape at the outboard 'shoulder'

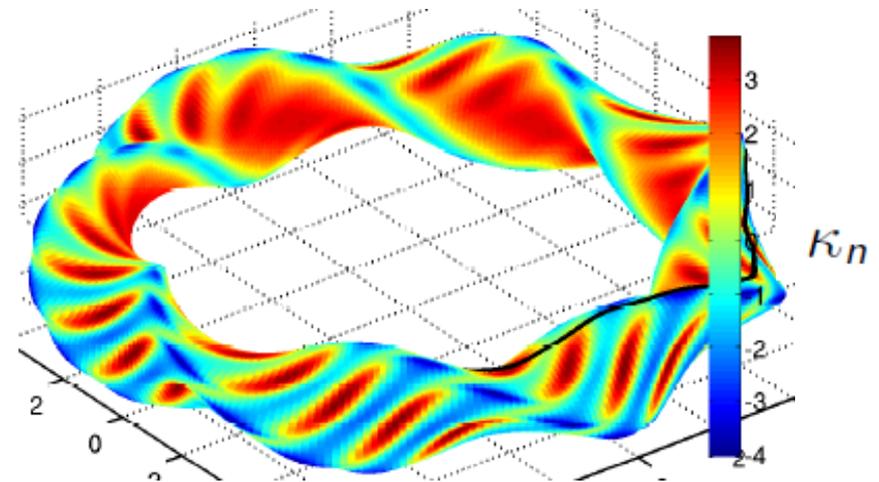
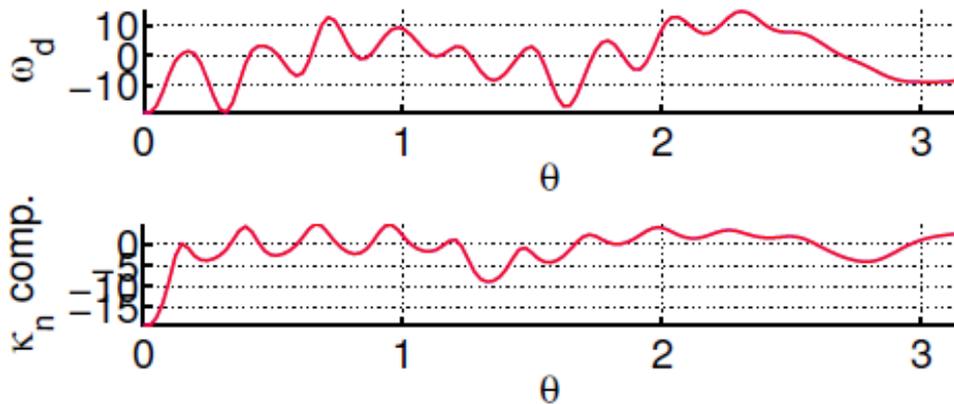


Keeping the torsion single-signed longer allows larger integrated shear: more stability.



Kinetic effects appear mostly unimportant in these parameter regimes

- Analytic model tracks trends despite lacking resonant kinetic contributions
 - Possible explanations:
 - Not in the right parameter regime -- only important near threshold?
 - Modes too extended -- i.e. need smaller λ_{\parallel} ?
 - Investigation with numerical experiments:



Even with connection length approx. 10x shorter than tokamak, proxy still accurately tracks GENE trends

Conclusions

i. Fluid-based targets have been investigated

- Scale generally with curvature and FLR terms

ii. Framework for geometric understanding shown

- Symmetry patterns dictated by edge locations in 3-D
 - May be fundamentally altered & tailored via shaping

iii. Analytic model predicts GENE trends

- Mode width important in proxy, less so in GENE

iv. Results suggest continuum of shaping effects

- Geodesic curvature-torsion optimization shows promise

v. Results translate directly to STELLOPT proxy & output analysis

Future work

Shortest term

- Write up results for paper & do prelim
- Translate proxy for current STELLOPT implementation (Mynick et. al.)
- Support & collaborate in HSX optimization inquiries

Medium term

- More analytic focus – helps untangle large parameter space
 - Analytic proxies for TEM type modes & kinetic effects
 - Better estimates of mode lengths
 - Better understanding of global behavior (one tube vs. another)

Longer term

- Nonlinear optimization targets -- existence, implications, etc.
 - Can the nonlinear physics be optimized?